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Title: Producing the Fission-Product-Isotope File KIDMAN

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# Los Alamos

Los Alamos National Laboratory  
Los Alamos, New Mexico 87545

# memorandum

TO: R. C. Little, X-6, MS B226

DATE: 15-September-1989

FROM: R. E. Seamon, X-6

MAIL STOP/TELEPHONE: B226 / 7-4809

SYMBOL: X-6:RES-89-340

SUBJECT: Producing the Fission-Product-Isotope File KIDMAN

In Ref. 1 I described the CFS file /076997/MYREDSTUFF/KIDMAN, an ACE file for the Monte Carlo code MCNP (Ref. 2) containing transport cross sections for twenty six fission product isotopes from ENDF/B-V. There is a second file associated with KIDMAN, the directory file stored under /076997/MYREDSTUFF/KIDMAND.

I found that Bob MacFarlane, T-2, had processed the evaluations through the RESR and UN-RESR modules of NJOY (Ref. 3) to produce PENDF files; there were no ACER files available for any of the isotopes, however. Starting from the PENDF file and the BCD ENDF/B-V tape indicated in Table II of Ref. 1, I used the HEATR and ACER modules of NJOY to produce what are alleged to be Type 3 ACE files which should be useable in MCNP and related checking codes. Nothing would work; the problem was traced to extra record marks which had to be removed using the code FIXACEFILE. I took the opportunity to remove as well the completely unnecessary photon production matrix ( $30 \times 20$  zero values) at the end of each file. There is no photon production data for any of the 26 isotopes; I am unable to run the ACER module in such a way that the zeroes would disappear.

The corrected ACE files were processed through ADDXS (Ref. 4) to add charged-particle-production cross sections for eleven of the isotopes where it was appropriate, and the individual files were merged using your version of Pat Soran's original code CULIT (Ref. 5). Checks were made using XDATAP (Ref. 6), MARK and MRKACR (Ref. 7), and FISHPC (Ref. 4).

The purpose of this memo is to document explicitly how this work was done, or – more truthfully – how I would do the job again knowing what I know now. First, the codes will be listed, then the data decks, and – finally – what problems were encountered.

The codes -- --

NJOY: Based on experiences in processing the excited-state data for Dave Madland, I chose to use the binary executable version of NJOY stored on CFS under /NJOY/89/XNJOY0.

FIXACEFILE: The source for this code is stored on CFS under /076997/MYREDSTUFF /FIX-ACEFILE. A listing thereof is given in Appendix A. Let CODE=FIXACEFILE; one gets the binary executable file XCODE using RCFT I=CODE,GO.

ADDXS: The source is stored on CFS under /090895/CTSS/ADDXS. One gets the binary executable XADDXS using RCFT I=ADDXS,GO.

CUL: The source is stored on CFS under /MYREDSTUFF/CUL. One gets the binary executable XCUL using RCFT I=CUL,GO.

XDATAP: I use the binary version which has grown out of my collaboration with Harl'O Fisher on the *Handbook*; it is stored on CFS under /076997/MYREDSTUFF/XDATAP6.

FISHPC: The source is stored on CFS under /090895/CTSS/FISHPC. One gets the binary executable XFISHPC using RCFT I=FISHPC,LIB=(CFTLIB,SCCF,CGSCFT),GO.

MARK: The source is stored on CFS under /076997/PGMS/MARK. One gets the binary executable XMARK using RCFT I=MARK,GO.

MRKACR: The source is stored on CFS under /076997/PGMS/MRKACR. One gets the binary executable XMRKACR using RCFT I=MRKACR,GO.

The input decks ---

NJOY: Here is a listing of the file INPUT associated with the NJOY run for Xe-131.

```
0
5
*MODER*
20 -21
*HEATR*
-21 -23 -28
1351 0 0 0 0 2 /
*ACER*
-21 -28 0 -30 31 /
0 1351 300.0 1 0
0.001 32 /
-1 5000 1.0E10
*STOP*
```

ENDF/B-V BCD input Tape20 was /ENDF/5/A/T/509.

Binary PENDF Tape23 was /PENDF/5/XE/131.

MAT = 1351

Binary Tape30 is the pseudo ACE-formatted file - "pseudo" because of those miserable extra record marks.

FIXACEFILE: No input file is needed. Binary Tape30 is the pseudo ACE file to be corrected and binary Tape31 - a real ACE file - is produced.

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ADDXS: Here is a listing of the TAPE8 input file appropriate for Pr<sup>141</sup>, Nd<sup>143</sup>, Nd<sup>145</sup>, Nd<sup>148</sup>, Pm<sup>147</sup>, Sm<sup>147</sup>, Sm<sup>151</sup>, Sm<sup>152</sup>, and Eu<sup>155</sup>. The format is 2I5.

	5
203	2
28	103
204	1
104	
205	1
105	
206	1
106	
207	2
22	107

CUL: Here is a listing of the CULINP file for a run in which I merged HERFILE containing 25 ZAIDs with file 9832B containing one ZAID (=63155.50). In this run the output file MYFILE became the final file KIDMAN. These lines start in column 1.

MYFILE
2
HERFILE
9832B
40093.50
42095.50
43099.50
44101.50
44103.50
45105.50
46105.50
46108.50
53135.50
.
.
.
.
59141.50
61148.50
61149.50
62147.50
62150.50
62151.50
62152.50
63155.50
0.

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FISHPC: Requires that KIDMAN be SWITCHed to EXTRA and that input file XSIN be one blank line.

MARK and MRKACR: The file INPUT is stored on CFS under /076997/R028/MARKD. For MARK, Tape7 must be the BCD File3 data; for MRKACR Tape7 is an ACE file like KIDMAN.

Additional Remarks ---

Before I merged the individual ACE files using CUL, I changed the ZAIDs manually using EDIT so that they would have suffix  $nn = 50$  in ZAID=ZZAAA.nn. Locations 1<sub>s</sub> and 312<sub>s</sub> in file OUTACE from ADDXS were changed.

There was a threshold problem discovered in Xe<sup>131</sup> MAT=1351, MT=51 when I ran MRKACR. For reasons unknown to me, NJOY is no longer shifting the thresholds for inelastic scattering to insure that

$$E_{th} \geq |Q| \frac{AWR + 1.0}{AWR}.$$

Specifically, for MAT=1351, MT=51  $E_{th} = 8.0616400E-02$  while EC=8.0616423051140E-02. Clearly, E can be less than EC in the interval  $E_{th} \leq E \leq EC$ . I changed EC using EDIT to 8.061600E-02 to eliminate that problem. In subsequent runs with MCNP in which I transported neutrons through Xe<sup>131</sup> there were no negative-energy secondary neutrons produced.

There were eleven isotopes (Xe<sup>135</sup>, Tc<sup>99</sup>, Pr<sup>141</sup>, Nd<sup>145</sup>, Nd<sup>143</sup>, Nd<sup>148</sup>, Eu<sup>155</sup>, Pm<sup>147</sup>, Sm<sup>147</sup>, Sm<sup>151</sup>, Sm<sup>152</sup>) for which some of the reaction cross sections were given in terms of the semi-log interpolation INT=3 on the ENDF/B-V tapes. This interpolation code (y linear in ln x) is not handled in MARK because closed-form expressions cannot be written for the integrals. Therefore, I was forced to rely on the ACE/ENDF comparison plots produced with XDATAP to check the NJOY processing of the cross sections for these reactions. The INT=3 cross sections have scallops on log-log plots. That only increased my apprehension and I decided to reproduce one of MacFarlane's PENDF tapes starting from "scratch." The deck for that NJOY run is listed here.

```
0
5
*MODER*
20 -21
*RECONR*
-21 -22
*PENDF TAPE FOR XE-135 ON TAPE 509* /
1294 0 0/
0.001 0.0 6/
0/
*BROADR*
-22 -23
1294 1 0 0 0.0 /
0.001 1.0E+06 /
300.0 /
0/
*HEATR*
-21 -23 -28
1294 0 0 0 0 2/
*ACER*
-21 -28 0 -30 31 /
0 1294 300. 1 0
0.001 32/
-1 5000 1.0E+10
*STOP*
```

I was processing  $Xe^{135}$  MAT=1294 on Tape509. Tape509 was Tape20 in this run. The NJOY outputs for this full run and the "short" run started from the PENDF tape are available in Appendix B. The final ACE files were not identical; I had roughly twice as many points in "my" output ACE file. However, the MRKACR output striped to three and four significant figure agreement and the plots produced in XDATAP run in COMPARE mode were indistinguishable. On the basis of this experience with the one isotope I decided to start my processing from MacFarlane's PENDF tapes – those listed in Table II of Ref. 1. This is not a confession, however, because – after all – I have compared all of the final ACE files on KIDMAN with the original ENDF/B-V cross sections.

Three MCNP runs have been made using KIDMAN. A copy of the first page of each of the runs is included in Appendix C.

I intend to hold on to all the plots and MARK/MRKACR outputs for a while. They are stored in the middle drawer of the filing cabinet in my office under KIDMAN Service Job. The microfiche listings from KIDMAN will be saved to become a permanent addition to our fiche library.

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## REFERENCES

1. R. E. Seamon, "Fission-Product-Isotope Cross Sections in ACE Format for MCNP," Los Alamos National Laboratory internal memorandum to R. B. Kidman (September 13, 1989).
2. J. F. Briesmeister, editor, "MCNP - A General Monte Carlo Code for Neutron and Photon Transport Version 3A," Los Alamos National Laboratory manual LA-7396-M, Rev. 2 (September 1986).
3. R. E. MacFarlane, D. W. Muir, and R. M. Boicourt, "The NJOY Nuclear Data Processing System, Volume I: User's Manual," Los Alamos National Laboratory manual LA-9303-M, Vol. I (ENDF-324) (May 1982).
4. R. C. Little, "Cross Section Processing Codes on the CRAY," Los Alamos National Laboratory internal memorandum X-6:RCL-85-415 to R. E. Seamon and H. M. Fisher (August 13, 1985).
5. R. C. Little, "The Code CUL," Los Alamos National Laboratory internal memorandum to R. E. Seamon (February 1, 1984).
6. H. M. Fisher, "XDATAP," Los Alamos National Laboratory report LA-11155-MS (October 1987).
7. R. E. Seamon, "The MARK and MRKACR Codes," Los Alamos National Laboratory internal memorandum X-6:RES-87-182 to Distribution (March 26, 1987).

## DISTRIBUTION

R. C. Little, X-6, MS B226  
H. M. Fisher, X-6, MS B226  
X-6 Files, MS B226 (2)

RES:res

## APPENDIX A

### Listing of CFS File /076997/MYREDSTUFF/FIXACEFILE

```
1      PROGRAM MUCK(TAPE30=0,TAPE31=0)
2      DIMENSION GREAT(2048),IGREAT(2048)
3      EQUIVALENCE(GREAT(1),IGREAT(1))
4      INTEGER EXTRA
5      IDA=1
6      IDB=1
7      CALL RDISK(30,GREAT,5,IDA)
8      IF(UNIT(30)) 299,299,350
9      299 LENGTH=IGREAT(4)
10     N=LENGTH/2048
11     EXTRA=LENGTH-2048*N + N
12     NEWLGT=2048*N + EXTRA - 600
13     M=NEWLGT/2048
14     EXTRA=NEWLGT - M*2048
15     IF(M.EQ.0) GO TO 4
16     CALL RDISK(30,GREAT,2048,IDA)
17     IF(UNIT(30)) 300,300,350
18     300 IGREAT(221)=IGREAT(221)-600
19     IGREAT(4)=201+IGREAT(221)+4
20     CALL WDISK(31,GREAT,2047,IDB)
21     IF(UNIT(31)) 301,301,350
22     301 IDA=IDA+2048
23     IDB=IDB+2047
24     IF(M.EQ.1) GO TO 3
25     DO 1 I=2,M
26     CALL RDISK(30,GREAT,2048,IDA)
27     IF(UNIT(30)) 302,302,350
28     302 CALL WDISK(31,GREAT,2047,IDB)
29     IF(UNIT(31)) 303,303,350
30     303 IDA=IDA+2048
31     IDB=IDB+2047
32     1 CONTINUE
33     3 CALL RDISK(30,GREAT,EXTRA,IDA)
34     IF(UNIT(30)) 304,304,350
35     304 CALL WDISK(31,GREAT,EXTRA,IDB)
36     IF(UNIT(31)) 305,305,350
37     4 CALL RDISK(30,GREAT,EXTRA,IDA)
38     IF(UNIT(30)) 306,306,350
39     306 IGREAT(221)=IGREAT(221)-600
40     IGREAT(4)=201+IGREAT(221)+4
41     CALL WDISK(31,GREAT,EXTRA,IDB)
42     IF(UNIT(31)) 307,307,350
43     307 STOP
44     305 STOP
45     350 STOP 765
46     END
```

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## APPENDIX B

## Two NJOY Output Files

MAT=1294 Straight Through NJOY

ERRINT FOR THINNING ..... 1.00000E-07  
FINAL TEMPERATURES ..... 3.00E+02

MAX ENERGY FOR BROADENING AND THINNING = 5.30942E+05  
BROADENED MAT1294 FROM 0.0000E+00 TO 3.0000E+02 K 2.1285  
POINTS IN= 778 POINTS OUT= 720 MT 2 102 4.2635

\*\*\*\*\*  
HEATR...PROMPT KERMA 4.2805  
\*\*\*\*\*

INPUT ENDF/B UNIT .....  
INPUT PENDF UNIT .....  
OUTPUT PENDF UNIT .....  
MAT TO BE PROCESSED .....  
NO. TEMPERATURES (0=ALL) 0  
GAMMA HEAT (0 NONLOCAL, 1 LOCAL) 0  
PRINT OPTION (0 MIN, 1 MORE, 2 CHK) .. 1

NO PHOTON PRODUCTION FILES... ALL PHOTON ENERGY WILL BE DEPOSITED LOCALLY.

PROCESSING AT TEMPERATURE= 3.0000E+02

NEUTRON HEATING FOR MT	2	Q0 = 0.0000E+00	Q = 0.0000E+00
E	EBAR	XSEC	HEATING
1.0000E-05	9.8528E-06	1.0011E+06	1.4749E-01
1.0962E-04	1.0801E-04	3.5097E+05	5.6680E-01
1.0962E-03	1.0801E-03	2.1893E+05	3.5357E+00
1.1927E-02	1.1751E-02	2.4029E+05	4.2222E+01
1.2000E-01	1.1823E-01	3.8641E+05	6.8312E+02
1.2098E+00	1.1920E+00	1.6388E+03	2.9209E+01
2.4395E+00	2.4036E+00	4.2106E+02	1.5133E+01
4.8985E+00	4.8263E+00	4.2541E+02	9.0501E+00
9.8000E+00	9.6556E+00	4.5469E+01	6.5647E+00
2.0000E+01	1.9705E+01	2.0804E+01	6.1300E+00
4.0000E+01	3.9411E+01	1.2701E+01	7.4844E+00
8.0000E+01	7.8821E+01	9.5476E+00	1.1253E+01
1.6000E+02	1.5764E+02	8.1941E+00	1.9315E+01
3.2000E+02	3.1529E+02	7.5720E+00	3.5697E+01
6.5414E+02	6.4450E+02	7.2754E+00	7.0114E+01
1.3218E+03	1.3023E+03	1.8817E+01	3.6607E+02
2.7244E+03	2.6844E+03	1.4056E+01	5.6278E+02
5.4584E+03	5.3784E+03	1.0975E+01	8.7861E+02
1.1007E+04	1.0846E+04	8.8481E+00	1.4166E+03
2.4000E+04	2.3660E+04	7.2191E+00	2.4527E+03
5.0000E+04	4.9311E+04	6.2551E+00	4.3124E+03
1.0000E+05	9.8723E+04	5.6934E+00	7.2728E+03
2.0000E+05	1.9776E+05	5.4419E+00	1.2164E+04
4.5000E+05	4.4575E+05	5.6629E+00	2.4042E+04
6.0344E+05	5.9801E+05	5.8818E+00	3.1907E+04
8.1067E+05	8.0393E+05	6.1172E+00	4.1249E+04
1.0000E+06	9.9212E+05	6.2712E+00	4.9427E+04
1.2200E+06	1.2111E+06	6.2479E+00	5.6023E+04
1.4076E+06	1.3978E+06	6.1122E+00	5.9952E+04
1.6000E+06	1.5894E+06	5.9057E+00	6.2577E+04
1.8430E+06	1.8315E+06	5.4978E+00	6.3285E+04

6.	3.393E+00
6.	3.569E+04
6.	4.413E+00
6.	4.703E+04
6.	4.992E+04
6.	5.389E+00
7.	3.389E+00
7.	3.897E+00
7.	4.074E+00
7.	4.718E+00
7.	5.442E+00
7.	6.030E+00
7.	6.955E+00
7.	7.994E+00
8.	8.042E+00
9.	9.182E+00
1.	1.000E+07
1.	1.122E+07
1.	1.193E+07
1.	1.339E+07
1.	1.344E+07
1.	1.420E+07
1.	1.416E+07
1.	1.495E+07
1.	1.500E+07
1.	1.616E+07
1.	1.732E+07
1.	1.859E+07
1.	1.866E+07
2.	2.000E+07
3.	3.964E+00
3.	3.964E+00
4.	4.262E+00
4.	4.413E+00
4.	4.839E+00
4.	5.323E+00
4.	5.529E+00
4.	5.614E+00
4.	5.724E+00
4.	5.831E+00
4.	5.931E+00
4.	6.031E+00
4.	6.131E+00
4.	6.231E+00
4.	6.331E+00
4.	6.431E+00
4.	6.531E+00
4.	6.631E+00
4.	6.731E+00
4.	6.831E+00
4.	6.931E+00
4.	7.031E+00
4.	7.131E+00
4.	7.231E+00
4.	7.331E+00
4.	7.431E+00
4.	7.531E+00
4.	7.631E+00
4.	7.731E+00
4.	7.831E+00
4.	7.931E+00
4.	8.031E+00
4.	8.131E+00
4.	8.231E+00
4.	8.331E+00
4.	8.431E+00
4.	8.531E+00
4.	8.631E+00
4.	8.731E+00
4.	8.831E+00
4.	8.931E+00
4.	9.031E+00
4.	9.131E+00
4.	9.231E+00
4.	9.331E+00
4.	9.431E+00
4.	9.531E+00
4.	9.631E+00
4.	9.731E+00
4.	9.831E+00
4.	9.931E+00
4.	1.000E+01
5.	1.988E+06
5.	2.527E+06
5.	2.983E+06
5.	3.532E+06
5.	4.013E+06
5.	4.572E+06
5.	5.000E+06
5.	6.098E+06
5.	7.000E+06
5.	7.995E+06
5.	8.995E+06
5.	9.947E+06
5.	1.042E+07
5.	1.134E+07
5.	1.252E+07
5.	1.317E+07
5.	1.416E+07
5.	1.500E+07
5.	1.616E+07
5.	1.732E+07
5.	1.859E+07
5.	1.866E+07
6.	2.000E+07
6.	2.420E+07
6.	2.647E+00
6.	2.781E+00
6.	3.065E+00
6.	3.230E+00
6.	3.296E+00
6.	3.396E+00
6.	3.496E+00
6.	3.596E+00
6.	3.696E+00
6.	3.796E+00
6.	3.896E+00
6.	3.996E+00
6.	4.096E+00
6.	4.196E+00
6.	4.296E+00
6.	4.396E+00
6.	4.496E+00
6.	4.596E+00
6.	4.696E+00
6.	4.796E+00
6.	4.896E+00
6.	4.996E+00
6.	5.096E+00
6.	5.196E+00
6.	5.296E+00
6.	5.396E+00
6.	5.496E+00
6.	5.596E+00
6.	5.696E+00
6.	5.796E+00
6.	5.896E+00
6.	5.996E+00
6.	6.096E+00
6.	6.196E+00
6.	6.296E+00
6.	6.396E+00
6.	6.496E+00
6.	6.596E+00
6.	6.696E+00
6.	6.796E+00
6.	6.896E+00
6.	6.996E+00
6.	7.096E+00
6.	7.196E+00
6.	7.296E+00
6.	7.396E+00
6.	7.496E+00
6.	7.596E+00
6.	7.696E+00
6.	7.796E+00
6.	7.896E+00
6.	7.996E+00
6.	8.096E+00
6.	8.196E+00
6.	8.296E+00
6.	8.396E+00
6.	8.496E+00
6.	8.596E+00
6.	8.696E+00
6.	8.796E+00
6.	8.896E+00
6.	8.996E+00
6.	9.096E+00
6.	9.196E+00
6.	9.296E+00
6.	9.396E+00
6.	9.496E+00
6.	9.596E+00
6.	9.696E+00
6.	9.796E+00
6.	9.896E+00
6.	9.996E+00
6.	1.000E+01

NEUTRON HEATING FOR MT 51		Q0 = 0.0000E+00	Q = -5.2700E+05
E	EBAR	XSEC	HEATING
6.0344E+05	7.0441E+04	2.1975E-02	1.1713E+04
8.1067E+05	2.7449E+05	6.7409E-02	3.6143E+04
1.0000E+06	4.6105E+05	1.0089E-01	5.4375E+04
1.2200E+06	6.7798E+05	1.3171E-01	7.1398E+04
1.4076E+06	8.6306E+05	1.4939E-01	8.1353E+04
1.6000E+06	1.0522E+06	1.6200E-01	8.8750E+04
1.8430E+06	1.2926E+06	1.5590E-01	8.5805E+04
2.0000E+06	1.4470E+06	1.5237E-01	8.4265E+04
2.5417E+06	1.9800E+06	1.0502E-01	5.8984E+04
3.0000E+06	2.4321E+06	6.6016E-02	3.7488E+04
3.5529E+06	2.9771E+06	4.6476E-02	2.6761E+04
4.0413E+06	3.4577E+06	3.1600E-02	1.8440E+04
4.5724E+06	3.9808E+06	1.7336E-02	1.0256E+04
5.0000E+06	4.4021E+06	7.0103E-03	4.1917E+03
6.0698E+06	5.4561E+06	3.5621E-03	2.1861E+03
7.0000E+06	6.3736E+06	1.0262E-03	6.4278E+02
8.4265E+06	7.3992E+06	6.4746E-04	4.1616E+02
9.1826E+06	8.5237E+06	2.8546E-04	1.8808E+02
1.0000E+07	9.3287E+06	5.2721E-05	3.5389E+01
1.1221E+07	1.0533E+07	2.3587E-05	1.6239E+01
1.2000E+07	1.1293E+07	6.6274E-06	4.6452E+00
1.3444E+07	1.2723E+07	5.3755E-06	3.8792E+00
1.4208E+07	1.3474E+07	4.7668E-06	3.4968E+00
1.5000E+07	1.4256E+07	4.1692E-06	3.1028E+00
1.6161E+07	1.5339E+07	3.3480E-06	2.5509E+00
1.7338E+07	1.6600E+07	2.5466E-06	1.9872E+00
1.8666E+07	1.7836E+07	1.7643E-06	1.4097E+00
2.0000E+07	1.9182E+07	1.0000E-06	8.1796E-01

  

NEUTRON HEATING FOR MT 91		Q0 = 0.0000E+00	Q = -5.2700E+05
E	EBAR	XSEC	HEATING
1.2200E+06	1.4211E+05	9.3509E-02	1.0080E+05
1.4076E+06	2.5573E+05	2.3120E-01	2.6632E+05
1.6000E+06	3.5467E+05	4.0482E-01	5.0008E+05
1.8430E+06	4.9100E+05	6.9162E-01	9.3508E+05
2.0000E+06	5.6576E+05	8.5743E-01	1.2298E+06
2.5417E+06	7.8255E+05	1.3722E+00	2.4150E+06
3.0000E+06	9.1869E+05	1.6738E+00	3.4837E+06
3.5529E+06	1.0334E+06	1.7325E+00	4.3652E+06
4.0413E+06	1.0992E+06	1.7773E+00	5.2289E+06

NEUTRON HEATING FOR MT 102		Q0 = 7.8800E+06	Q = 7.8800E+06
E	EBAR	XSEC	HEATING
1.0000E-05	0.0000E+00	8.8795E+07	6.9970E+14
1.0962E-04	0.0000E+00	2.6883E+07	2.1184E+14
1.0962E-03	0.0000E+00	8.6203E+06	6.7928E+13
1.1927E-02	0.0000E+00	3.0903E+06	2.4351E+13
1.2000E-01	0.0000E+00	1.5712E+06	1.2381E+13
1.2098E+00	0.0000E+00	1.8894E+03	1.4888E+10
2.4395E+00	0.0000E+00	3.0596E+02	2.4110E+09
4.8985E+00	0.0000E+00	5.2446E+01	4.1328E+08
9.8000E+00	0.0000E+00	9.6032E+00	7.5674E+07
2.0000E+01	0.0000E+00	1.9513E+00	1.5376E+07
4.0000E+01	0.0000E+00	5.8812E-01	4.6344E+06
8.0000E+01	0.0000E+00	2.7660E-01	2.1796E+06
1.6000E+02	0.0000E+00	1.7104E-01	1.3478E+06
3.2000E+02	0.0000E+00	1.1660E-01	9.1887E+05
6.5414E+02	0.0000E+00	8.0814E-02	6.3687E+05
1.3218E+03	0.0000E+00	5.4625E-02	4.3052E+05
2.7244E+03	0.0000E+00	3.0608E-02	2.4127E+05
5.4584E+03	0.0000E+00	1.7205E-02	1.3567E+05
1.1007E+04	0.0000E+00	9.9610E-03	7.8595E+04
2.4000E+04	0.0000E+00	5.6940E-03	4.5006E+04
5.0000E+04	0.0000E+00	3.4800E-03	2.7597E+04
1.0000E+05	0.0000E+00	2.1950E-03	1.7516E+04
2.0000E+05	0.0000E+00	1.5490E-03	1.2516E+04
4.5000E+05	0.0000E+00	1.2480E-03	1.0396E+04
1.0076E+06	0.0000E+00	4.4206E-04	4.1057E+03
2.4000E+06	0.0000E+00	4.2460E-04	4.0252E+03
6.0344E+05	0.0000E+00	7.9413E-04	6.7369E+03
1.6000E+06	0.0000E+00	5.9043E-04	5.1312E+03
4.0413E+06	0.0000E+00	4.0033E-04	3.8924E+03
2.0000E+06	0.0000E+00	3.8630E-04	3.8166E+03
2.5411E+06	0.0000E+00	3.3242E-04	4.8023E+03
3.0000E+06	0.0000E+00	2.7900E-04	3.4644E+03
6.0698E+06	0.0000E+00	1.5378E-03	1.9243E+04
7.0000E+06	0.0000E+00	1.5700E-03	2.1452E+04
3.5529E+06	0.0000E+00	6.8135E-04	2.3362E+04
1.8430E+06	0.0000E+00	9.8766E-04	7.7898E+03
2.0000E+06	0.0000E+00	1.2814E-03	1.1774E+04
4.5724E+06	0.0000E+00	1.4940E-03	1.5956E+04
5.0000E+06	0.0000E+00	1.4940E-03	1.9243E+04
6.0698E+06	0.0000E+00	1.5378E-03	2.1452E+04
7.0000E+06	0.0000E+00	1.5700E-03	2.3362E+04
8.0420E+06	0.0000E+00	1.6805E-03	2.6757E+04
9.1826E+06	0.0000E+00	1.7861E-03	3.0476E+04
1.0000E+07	0.0000E+00	1.8540E-03	3.3150E+04
1.1221E+07	0.0000E+00	2.0089E-03	3.8372E+04
1.2000E+07	0.0000E+00	2.0930E-03	4.1728E+04

1.3444E+07	0.0000E+00	2.3093E-03	4.9245E+04
1.4208E+07	0.0000E+00	2.4116E-03	5.3261E+04
1.5000E+07	0.0000E+00	2.5120E-03	5.7475E+04
1.6161E+07	0.0000E+00	2.3793E-03	5.7201E+04
1.7380E+07	0.0000E+00	2.2499E-03	5.6832E+04
1.8660E+07	0.0000E+00	2.1235E-03	5.6356E+04
2.0000E+07	0.0000E+00	2.0000E-03	5.5760E+04
FINAL KERMA FACTORS			
	E	301	
1.0000E-05	MIN	6.7373E+00	
	MAX	6.9970E+14	
	HIGH	2.1776E+10	
1.0962E-04	MIN	2.2436E+01	
	MAX	2.1184E+14	
	HIGH	6.5928E+09	
1.0962E-03	MIN	7.3664E+01	
	MAX	6.7928E+13	
	HIGH	2.1141E+09	
1.1927E-02	MIN	3.1575E+02	
	MAX	2.4351E+13	
	HIGH	7.5787E+08	
1.2000E-01	MIN	2.0823E+03	
	MAX	1.2381E+13	
	HIGH	3.8533E+08	
1.2098E+00	MIN	4.6173E+01	
	MAX	1.4888E+10	
	HIGH	4.6340E+05	
2.4395E+00	MIN	2.0672E+01	
	MAX	2.4110E+09	
	HIGH	7.5056E+04	
4.8985E+00	MIN	1.0957E+01	
	MAX	4.1328E+08	
	HIGH	1.2873E+04	
9.8000E+00	MIN	7.2631E+00	
	MAX	7.5674E+07	
	HIGH	2.3624E+03	
2.0000E+01	MIN	6.4196E+00	
	MAX	1.5376E+07	
	HIGH	4.8496E+02	
4.0000E+01	MIN	7.6590E+00	
	MAX	4.6344E+06	
	HIGH	1.5189E+02	

## HIGH

MIN 1.1417E+01  
8.0000E+01 2.1796E+06  
MAX 7.9252E+01  
HIGH

MIN 1.9518E+01  
1.6000E+02 1.3478E+06  
MAX 6.1465E+01  
HIGH

MIN 3.5974E+01  
3.2000E+02 9.1891E+05  
MAX 6.4573E+01  
HIGH

MIN 7.0506E+01  
6.5414E+02 6.3694E+05  
MAX 9.0328E+01  
HIGH

MIN 3.6660E+02  
1.3218E+03 4.3088E+05  
MAX 3.8000E+02  
HIGH

MIN 5.6340E+02  
2.7244E+03 2.4184E+05  
MAX 5.7091E+02  
HIGH

MIN 8.7931E+02  
5.4584E+03 1.3655E+05  
MAX 8.8353E+02  
HIGH

MIN 1.41174E+03  
1.1007E+04 8.00112E+04  
MAX 1.4198E+03  
HIGH

MIN 2.4537E+03  
2.4000E+04 4.7458E+04  
MAX 2.4551E+03  
HIGH

MIN 4.3137E+03  
5.0000E+04 3.1909E+04  
MAX 4.3146E+03  
HIGH

MIN 7.2745E+03  
1.0000E+05 2.4789E+04  
MAX 7.2750E+03  
HIGH

MIN 1.21166E+04  
2.0000E+05 2.4680E+04  
MAX 1.21167E+04  
HIGH

MIN 2.4047E+04  
4.5000E+05 3.4438E+04

		MAX	2.4047E+04	HIGH
6.0344E+05	MIN	3.2042E+04		
	MAX	5.0356E+04		
		HIGH	3.2042E+04	
8.1067E+05	MIN	4.1872E+04		
	MAX	8.2524E+04		
		HIGH	4.1872E+04	
1.0000E+06	MIN	5.0637E+04		
	MAX	1.0860E+05		
		HIGH	5.0637E+04	
1.2200E+06	MIN	5.8964E+04		
	MAX	2.3253E+05		
		HIGH	5.8965E+04	
1.4076E+06	MIN	6.5459E+04		
	MAX	4.1173E+05		
		HIGH	6.5459E+04	
1.6000E+06	MIN	7.1905E+04		
	MAX	6.5544E+05		
		HIGH	7.1906E+04	
1.8430E+06	MIN	7.9006E+04		
	MAX	1.0881E+06		
		HIGH	7.9006E+04	
2.0000E+06	MIN	8.3813E+04		
	MAX	1.3812E+06		
		HIGH	8.3814E+04	
2.5417E+06	MIN	1.0134E+05		
	MAX	2.5410E+06		
		HIGH	1.0134E+05	
3.0000E+06	MIN	1.1645E+05		
	MAX	3.5889E+06		
		HIGH	1.1645E+05	
3.5529E+06	MIN	1.3162E+05		
	MAX	4.4697E+06		
		HIGH	1.3162E+05	
4.0413E+06	MIN	1.4351E+05		
	MAX	5.3325E+06		
		HIGH	1.4351E+05	
	MIN	1.5586E+05		

4.5724E+06 MAX	6.3438E+06 1.5586E+05 HIGH
5.0000E+06 MAX	1.6471E+05 7.2003E+06 1.6471E+05 HIGH
6.0698E+06 MAX	1.8677E+05 8.5554E+06 1.8677E+05 HIGH
7.0000E+06 MAX	2.0017E+05 9.6422E+06 2.0017E+05 HIGH
8.0420E+06 MAX	2.2532E+05 1.0973E+07 2.2532E+05 HIGH
9.1826E+06 MAX	2.4558E+05 1.2352E+07 2.4558E+05 HIGH
1.0000E+07 MAX	2.5699E+05 1.3296E+07 2.5699E+05 HIGH
1.1221E+07 MAX	2.7151E+05 1.3958E+07 2.7151E+05 HIGH
1.2000E+07 MAX	2.7979E+05 1.4300E+07 2.7979E+05 HIGH
1.3444E+07 MAX	2.9709E+05 1.5371E+07 2.9709E+05 HIGH
1.4208E+07 MAX	3.0727E+05 1.5896E+07 3.0727E+05 HIGH
1.5000E+07 MAX	3.1899E+05 1.6415E+07 3.1899E+05 HIGH
1.6161E+07 MAX	3.4270E+05 1.7126E+07 3.4271E+05 HIGH

MIN	3.6766E+05						
1.7380E+07	1.7816E+07						
MAX	3.6766E+05	HIGH					
 MIN	3.9388E+05						
1.8660E+07	1.8481E+07						
MAX	3.9389E+05	HIGH					
 MIN	4.2141E+05						
2.00000E+07	1.9118E+07						
MAX	4.2142E+05	HIGH					
 MIN	4.9112E+05						
1.88800E+07	1.8481E+07						
MAX	4.9113E+05	HIGH					
 MIN	5.3575						
2.00000E+07	5.3575						
MAX	5.3575	HIGH					
 MIN	5.4415						
1.88800E+07	5.4415						
MAX	5.4415	HIGH					
 MIN	5.0000						
2.00000E+07	5.0000						
MAX	5.0000	HIGH					
 MIN	7399/ 120000						
1.88800E+07	7399/ 120000						
MAX	7399/ 120000	HIGH					
 MIN	720 WITH INTEGRALS						
1.88800E+07	720 WITH INTEGRALS						
MAX	720 WITH INTEGRALS	HIGH					
 MIN	9.6085E+07						
1.88800E+07	9.6085E+07						
MAX	9.6085E+07	HIGH					
 MIN	4.7305E+05						
1.88800E+07	4.7305E+05						
MAX	4.7305E+05	HIGH					
 MIN	27/ 11100						
1.88800E+07	27/ 11100						
MAX	27/ 11100	HIGH					
 ORIGINAL GRID=	720 WITH INTEGRALS						
1.88800E+07	720 WITH INTEGRALS						
MAX	720 WITH INTEGRALS	HIGH					
 NEW GRID=	562 WITH INTEGRALS						
1.88800E+07	562 WITH INTEGRALS						
MAX	562 WITH INTEGRALS	HIGH					
 NEW GRID=	690 WITH INTEGRALS						
1.88800E+07	690 WITH INTEGRALS						
MAX	690 WITH INTEGRALS	HIGH					
 TOTAL	2.1954E+04						
1.6976E-03	2.1954E+04						
1.5202E-01	4.1737E+05						
5.4000E-01	7.2586E+04						
2.3479E+00	8.4242E+03						
1.0464E+01	1.4454E+03						
8.4000E+01	1.1257E+03						
1.0012E+03	6.9913E+03						
1.0701E+05	7.2841E+05						
2.1939E+06	1.2852E+07						
2.0000E+07	8.1975E+07						
 CAPTURE	2.1535E+04						
1.6976E-03	2.1535E+04						
1.5202E-01	3.5750E+05						
5.4000E-01	5.4035E+04						
2.3479E+00	4.8740E+03						

MOVED E = 1.00000E+03 FOR MF= 4 MT= 2 12.7245

## Simple NJOY Run Starting from a PENDF Tape

2.8000E-01	2.2563E+05	0.0	0.0
9.4000E-01	1.5266E+04	0.0	0.0
4.6000E+00	1.9830E+03	0.2	0.0
1.8000E+01	1.6830E+02	0.3	0.0
1.6000E+02	5.7074E+01	0.1	0.0
2.0000E+04	3.5958E+02	0.0	0.0
1.3711E+06	1.3672E+03	0.0	0.0
2.0000E+07	3.2828E+04	0.0	0.0

37      39      39      39      37      38      38      39      39

REMOVED E= 1.00000E+03 FOR MF= 4 MT= 2

17.896S

\*\*\*\*\*

MCNP VERSION 3B5 LD=05/24/89 9406CP20N1 6 09/07/89 14:26:25  
 \*\*\*\*  
 INP=DON

```

1-      SERIES C RUN GAMMA-PRIME
2-      C   CELL CARDS FOR SPHERE CENTERED AT THE ORIGIN.
3-          1 1 1 -1
4-          2 0 #1
5-
6-      C   SURFACE CARDS
7-          1 SD .5
8-
9-      MODE N
10-     IMP:N 1 0
11-     SDEF ERG=20.0 POS=0 0 WGT=1 CEL=1
12-     FC1:N CURRENT ACROSS THE SURFACE OF THE U-235 SPHERE.
13-     F1:N 1
14-     F21:N 1
15-     FM21:N (1.0 2 (102))
16-     F41:N 1
17-     FM41:N (1.0 3 (2)(91))
18-     F61:N 1
19-     FM61:N (1.0 4 (53)(54)(55)(56)(57)(58))
20-     F81:N 1
21-     FMB1:N (1.0 5 (2) (2 102))
22-     F101:N 1
23-     FM101:N (1.0 6 (61)(62)(63)(64)(65)(66))
24-     F121:N 1
25-     FM121:N (1.0 2 (53:54)
26-     FC2:N FLUX ACROSS THE SURFACE OF THE U-235 SPHERE.
27-     F2:N 1
28-     F22:N 1
29-     FM22:N (1.0 2 (61)(62)(63)) (1.0 2 (54:55))
30-     FQE:M
31-     EO:N 1.0E-11 .025 .2 .235 .55 .7 1.0 2.0 81 20.0
32-     M1 4.0093 .50 0.01 4.2095 .50 0.40 60.43 50 0.39 63.155 .50 0.20
33-     M2 4.3099 .50 0.50 4.4101 .50 0.25 44.103 .50 0.25
WARNING. MATERIAL 2 IS USED ONLY FOR TALLYING.
34-     M3 4.5105 .50 1.0
WARNING. MATERIAL 3 IS USED ONLY FOR TALLYING.
35-     M4 4.6105 .50 1.0
WARNING. MATERIAL 4 IS USED ONLY FOR TALLYING.
36-     M5 4.6108 .50 1.0
WARNING. MATERIAL 5 IS USED ONLY FOR TALLYING.
37-     M6 4.4101 .50 1.0
WARNING. MATERIAL 6 IS USED ONLY FOR TALLYING.
38-     CUT:N 1.0E123 0.01
39-     PRINT
40-     NPS 7000
41-

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## APPENDIX C

### Three MCNP Runs for Testing KIDMAN

MCNP VERSION 3B5 LD=05/24/89 9406CP20N1 6 09/08/89 13:28:03  
\*\*\*\*\*  
INP=DON1

PRORID = 6 09/08/89 13:28:03  
  
1- C SERIES C RUN GAMMA-PRIME  
2- 3- 1 1 1 -1  
4- 2 0 #1  
5-  
6- C SURFACE CARDS  
7- 1 SD .5  
8-  
9- MODE N  
10- IMP:N 1 0  
11- SDEF ERG=20.0 POS=0 0 WGT=1 CEL=1  
12- FC1:N CURRENT ACROSS THE SURFACE OF THE U-235 SPHERE.  
13- F1:N 1  
14- F2:N 1  
15- FM2:N (1.0 2 (102))  
16- F4:N 1  
17- FM4:N (1.0 3 (2)(91))  
18- F6:N 1  
19- FM6:N (1.0 4 (53)(54)(55)(56)(57)(58))  
20- F8:N 1  
21- FMB1:N (1.0 5 (2) (2 102))  
22- F101:N 1  
23- FM101:N (1.0 6 (61)(62)(63)(64)(65)(66))  
24- F121:N 1  
25- FM121:N (1.0 2 (53:54))  
26- FC2:N FLUX ACROSS THE SURFACE OF THE U-235 SPHERE.  
27- F22:N 1  
28- F22:N 1  
29- FM22:N (1.0 7 (61)(62)(63)) (1.0 7 (54:55))  
30- FQE:M  
31- EO:N 1.0E-11 .025 .2 .235 .55 .7 1.0 2.0 81 20.0  
32- M1 53135 .50 0.01 54131 .50 0.40 59141 .50 0.39 54135 .50 0.20  
33- M2 43099 .50 0.50 44101 .50 0.25 44103 .50 0.25  
WARNING. MATERIAL 2 IS USED ONLY FOR TALLYING.  
34- M3 45105 .50 1.0  
WARNING. MATERIAL 3 IS USED ONLY FOR TALLYING.  
35- M4 46105 .50 1.0  
WARNING. MATERIAL 4 IS USED ONLY FOR TALLYING.  
36- M5 61149 .50 1.0  
WARNING. MATERIAL 5 IS USED ONLY FOR TALLYING.  
37- M6 44101 .50 1.0  
WARNING. MATERIAL 6 IS USED ONLY FOR TALLYING.  
38- M7 63155 .50 1.0  
WARNING. MATERIAL 7 IS USED ONLY FOR TALLYING.  
39- CUT:N 1.0E123 0.01  
40- PRINT  
41- NPS 7000  
42-

MCNP VERSION 3B5 LD=05/24/89

9406CP20N1 6 09/08/89 13:37:00

FP0BT0 - 6 09/08/89 13:37:00

\*\*\*\*\*  
INP=DON2

1- SERIES C RUN GAMMA-PRIME  
2- C CELL CARDS FOR SPHERE CENTERED AT THE ORIGIN.  
3- 1 1 1 -1  
4- 2 0 #1  
5-  
6- C SURFACE CARDS  
7- 1 SO .5  
8-  
9- MODE N  
10- IMP:N 1 0  
11- SDEF ERG=20.0 POS=0 0 0 WGT=1 CEL=1  
12- FC1:N CURRENT ACROSS THE SURFACE OF THE U-235 SPHERE.  
13- F1:N 1  
14- F21:N 1  
15- FM21:N (1.0 2 (102))  
16- F41:N 1  
17- FM41:N (1.0 3 (2)(91))  
18- F61:N 1  
19- FM61:N (1.0 4 (53)(54)(55)(56)(57)(58))  
20- F81:N 1  
21- FM81:N (1.0 5 (2) (2 102))  
22- F101:N 1  
23- FM101:N (1.0 6 (61)(62)(63)(64)(65)(66))  
24- F121:N 1  
25- FM121:N (1.0 2 (53:54))  
26- FC2:N FLUX ACROSS THE SURFACE OF THE U-235 SPHERE.  
27- F2:N 1  
28- F22:N 1  
29- FM22:N (1.0 2 (61)(62)(63)) (1.0 2 (54:55))  
30- FQ E M  
31- EO:N 1.0E-11 .025 .2 .235 .55 .7 1.0 2.0 8I 20.0  
32- M1 62147.50 0.20 62151.50 0.20 62150.50 .2 62152.5 .2 63155.5 .2  
33- M2 60143.5 .25 60145.5 .25 61148.5 .25 61149.5 .25  
WARNING. MATERIAL 2 IS USED ONLY FOR TALLYING.  
34- M3 60147.50 1.0  
WARNING. MATERIAL 3 IS USED ONLY FOR TALLYING.  
35- M4 60148.50 1.0  
WARNING. MATERIAL 4 IS USED ONLY FOR TALLYING.  
36- M5 61149.50 1.0  
WARNING. MATERIAL 5 IS USED ONLY FOR TALLYING.  
37- M6 59141.50 1.0  
WARNING. MATERIAL 6 IS USED ONLY FOR TALLYING.  
38- CUT:N 1.0E123 0.01  
39- PRINT  
40- NPS 7000  
41-